68

LEVEL BOOK

744

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16 6 in.	21	3.46 6 in.	41	6.76.6 in	61	10.06.6 in.	81	13.36.6 in.
2	33.0	22	3 63.0	42	6.93.0	62	10.23.0	82	13.53.0
3	49.6	23	3.79.6	43	7.09 6	63	10.39.6	83	13.69.6
4	66.0	24	3.96.0	44	7.26.0	64	10.56.0	84	13.86.[illegible]
5	82.6	25	4 12.6	45	7 42.6	65	10.72.6	85	14.02.[illegible]
6	99.0	26	4.29.0	46	7.59.0	66	10.89.0	86	14.[illegible]
7	1.15.6	27	4.45.6	47	7.75.6	67	11.05.6	87	14.[illegible]5.6
8	1.32.0	28	4.62.0	48	7.92.0	68	11.22.0	88	[illegible]
9	1.48.6	29	4.78.6	49	8.08.6	69	11.38.6	89	[illegible]
10	1.65.0	30	4.95.0	50	8.25.0	70	11.55.0	90	[illegible]
11	1.81.6	31	5.11.6	51	8.41.6	71	11.71.6	91	[illegible].01.[illegible]
12	1.98 0	32	5.28.0	52	8.58.0	72	11.88.0	92	[illegible].18.0
13	2.14.6	33	5.44.6	53	8.74.6	73	12.04.6	93	[illegible] 34.6
14	2.31.0	34	5.61.0	54	8.91.0	74	12.21.0	94	[illegible]
15	2.47.6	35	5.77.6	55	9.07 6	75	12.37.6	95	[illegible]
16	2.64.0	36	5.94.0	56	9.24.0	76	12.54.0	96	15.[illegible]4.0
17	2.80.6	37	6.10.6	57	9.40.6	77	12.70.6	97	[illegible]
18	2.97.0	38	6.27.0	58	9.57.0	78	12.87.0	98	[illegible]
19	3.13.6	39	6.43.6	59	9.73.6	79	13.03.6	99	16.[illegible]3.[illegible]
20	3.30.0	40	6.60.0	60	9.90.0	80	13.20.0	100	16.50.0

Scotland Station Rd
North

Chester Township

CAVE ROAD T.H. 157

Return to L. J. McLaughlin
Co. Eng'r
Chardon, O

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INDEX

11-3-19 Hanna
Fair - Cold Drake

BENCH-MARKS

Sta.	B.S.	H.I.	F.S.	Elev.	
B.M. 1				1138.00	+ on S.E. Cor. N. Parapet of (cement) stone Culvert 30' E of ℄ E.R.R.
B.M. #1	2.80	1126.81		1124.01	+ on S.W. Cor stone door sill of Brick School House
T.P.	9.36	1135.06	1.11	1125.70	
T.P.	10.07	1144.35	0.78	1134.28	
T.P.	11.94	1155.50	0.79	1143.56	
T.P.	11.60	1166.57	0.53	1154.97	
B.M. #2			2.05	1164.52	On W. root 24" Cucumber 50' Rt. Sta. 9+55
T.P.	12.07	1177.61	1.03	1165.54	
T.P.	11.55	1187.81	1.35	1176.26	
T.P.	11.19	1197.72	1.28	1186.53	
T.P.	11.58	1209.22	0.08	1197.64	
T.P.	10.81				

✓

Sta	B.S.	H.I.	F.S.	Elev.	
		1209 22			
T.P.	11.80	1220 86	0.16	1209.06	
T.P.	10.34	1230 57	0.63	1220.23	
B.M.#3			3.24	1227.33	On S.E. root 18" Maple 24' Lt., Sta. 18+85
T.P.	11.46	1241 14	0.89	1229.68	
T.P.	9.02	1248 82	1.34	1239.80	
T.P.	2.68	1243 29	8.21	1240.61	
B.M.#4			1.18	1242.11	On S.W. root 12" Maple 15 Rt., Sta. 80+16 (?)
T.P.	1.75	1233 00	12.04	1231.25	
T.P.	2.26	1226 28	8.98	1224.02	
T.P.	2.06	1219 88	8.46	1217.82	
B.M.#5			3.09	1216.79	On N.E. root split Maple 29' Lt. Sta. 42+93

✓

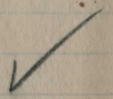
Sta.	B.S.	H.I.	F.S.	Elev.	
		1219.88			
T.P.	1.13	1210.80	10.21	1209.67	
T.P.	2.42	1201.09	12.13	1198.67	
T.P.	0.06	1189.22	11.93	1189.16	
B.M.#6			4.06	1185.16	On W. root 30" Oak 37' Lt., Sta. 56.
T.P.	3.13	1182.23	10.12	1179.10	
T.P.	8.09	1182.78	7.54	1174.69	
T.P.	3.23	1185.89	0.12	1182.66	
B.M.#7			7.18	1178.71	on N. root 14" Maple 27' Lt., Sta 96+12
T.P.	9.79	1193.49	2.19	1183.70	
T.P.	12.17	1205.33	0.33	1193.16	
T.P.	10.81	1215.79	0.35	1204.98	

✓

Sta.	B.S.	H.I.	F.S.	Elev.	
		1215.79			
T.P.	11.13	1226.22	0.70	1215.09	
T.P.	6.50	1231.31	1.41	1224.81	
B.M.#8			3.43	1227.88.	On W. root 18" Maple 24' Rt., Sta. 96
T.P.	1.59	1220.61	12.29	1219.02.	
T.P.	1.40	1209.96	12.05	1208.56	
T.P.	0.55	1198.59	11.92	1198.04	
T.P.	0.33	1187.61	11.31	1187.28	
T.P.	0.36	1176.42	11.55	1176.06	
T.P.	0.05	1165.41	11.06	1165.36	
B.M.#9		Rod slipped	(?) 11.94	5-8 1153.17	Fiedler on X Sec. [1153.58] On S.E. root 30" Maple 75' Rt., Sta. 109+25
T.P.	0.25	1154.65	11.01	1154.40	

✓

Sta.	B.S.	H.I.	F.S.	Elev.	
		1154	65		
T.P.	2.06	1150	70.	6.01	1148.64	
B.M. #10				5.27	1145.13	On E. root twin maple 26' Lt, Sta, 12+60
	+5.92	1157	04		1151.12	N.W. Corner Parcel St. Sta. 110+10
B.M. #9				-3.46	1153.58	



Fiedler Grove – Thompson
Nov. 6th 1919

Sta.	B.S.	H. I.	F.S.	Elev.
B.M.	2.62	1126.63	4.7	1124.01
0			4.7	21.9
+10	✓		4.4	22.2
+17	✓		4.2	22.4
1			4.7	21.9
+68				
+68	thru center line		4.7	21.9
2			4.8	21.8
3.			3.5	23.1
T.P.			2.31	1124.32
	+11.57	1135.89		
4			10.0	25.9

✓

Lt. R.T.

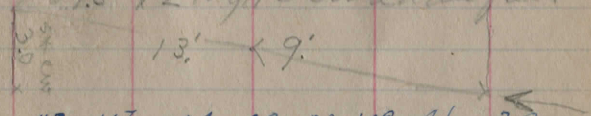
Sta. 0: −2.4 7.1/80. | 0.0 4.7 | +0.4 4.3/19. | +1.1 3.6/32. | +2.4 2.3/80.

Sta. +10: −3.6 8.0/80. | −1.8 6.2/36. | −1.0 5.4/12. | 0.0 4.4 | 0.0 4.4/25. | −0.4 4.8/36 | +0.6 3.8/80.

Sta. +17: −0.7 4.9/80. | +0.7 3.5/18 | −1.0 5.2/14. | 0.0 4.2 | −0.7 4.9/21. | +0.8 3.4/32 | +2.3 1.9/80

Sta. 1: 0.0 4.7/25+15. | −0.9 5.6/18. | −2.1 6.8/14 | −1.9 6.6/12. | −0.5 5.2/9. | 0.0 4.7 | −0.4 5.1/6 | −1.3 6.0/10. | −0.3 5.0/14. | −1.0 5.7/25

Box Culvert 2½' x 2½' x 22 long
Parapet 7' x 1.5' x 2' high – Condition fair



Sta. +68: −4.4 9.1/32. | −4.3 9.0/13. | +0.7 4.0/12. | −0.4 5.1/10. | 0.0 4.7 | 0.0 4.7/8. | +0.9 3.8/9. | −4.1 8.8/10. | −3.9 8.6/23. Fl. Tile

Sta. 2: −2.0 6.8/25. | −1.7 6.5/19. | −2.2 7.0/16. | −0.2 5.0/10. | 0.0 4.8 | −0.4 5.2/5. | −2.2 7./9. | −0.9 5.7/11. | −1.0 5.8/25.

Sta. 3: −0.5 4.0/25. | −0.6 4.1/21. | −1.5 5.0/18. | −0.2 3.7/15. | 0.0 3.5 | 0.0 3.5/2. | −1.5 5.0/5.0 | −0.1 3.6/7.+10. | +0.7 2.8/25.

Sta. 4: +0.5 9.5/25 | +0.6 9.4/21 | −0.6 10.6/18. | 0.0 10./16. | +0.2 9.8/10. | 0.0 10.0 | −0.7 10.7/3 | +0.7 9.3/5. | +2.4 7.6/25.

Sta.	B.S.	H.I.	F.S.	Elev.
		1138	89	
5			6.0	29.9
+15	South end 10" V.P. 3' R. of			
+21.8	South Rail. C & E			
	" " "		3.5	32.4
+29	N. end 15' sluice under V.P. 7'6" R. of ℄			
+15	✓		4.6	31.3
+40	✓		3.2	32.7
6			2.3	33.6
T.P.			−0.21	1135.68
	+9.92	1145.60		
7			7.1	38.5
T.P.			−0.36	1145.24
	+11.48	1156.72		
8.			9.5	47.2
9			0.3	56.4 ✓

+0.1 +0.1 −0.7 −0.2 0.0 −1.0 −0.1 +1.4 +2.0

5.2 5.9 6.7 6.2 7.0 6.1 4.6 4.0
25. 20. 16. 14. 6.0 2. 8. 14. 21.

−6.2 0.0 +1.0

4.68 3.5 2.52
30. 30.

−3.0

6.5 Flo Line
7.

−0.1 +0.3 −1.1 −0.3 0.0 −1.6 −1.2 −0.2 +1.1

4.7 4.8 5.7 4.9 4.6 6.2 5.6 4.8 5.5
25. 21. 17. 13. 2 5. 13. 25.

−1.4 −0.5 0.0 0.0 −1.3 −0.5 +0.2

4.6 3.7 3.2 3.2 4.5 3.7 3.0
25. 16. 3 2. 6. 10. 25.

−1.7 −1.1 −0.1 0.0 −0.1 −0.4 +0.8

4.0 3.4 2.4 2.3 2.7 2.7 1.5
25. 16. 9. 3. 8. 25.

−2.7 −2.0 +0.2 0.0 0.0 −0.1 −0.6

10. 7.1 6.9 7.1 7.2 7.7
25. 14. 9. 6. 7.1 6. 25.

−6.1 −5.5 −4.6 0.0 0.0 +0.5 −4.0 −3.0

15.6 15.0 11.1 9.5 9.0 13.5 12.5
30 25. 17 9 9.5 8. 15 25.

−9.7 −8.5 −8.1 −0.3 0.0 +2.3 −5.4

13.0 9.7 8.9 0.6 0.2 0.0 5.7
30. 25. 21. 9. 10. 2 + 30

Sta.	B.S.	H.I.	F.S.	Elev.
T.P.		1156.72	-0.25	1156.47
	+11.04	1167.51		
B.M. 2	+3.01	1167.53		1164.52
10			2.3	65.2
T.P.			-0.62	1166.91
	+12.15	1179.06		
11			4.0	75.1
T.P.			-0.62	1175.44
	+10.81	1189.25		
12			6.5	82.8
T.P.			-0.15	1159.10
	+1.32	1200.42		
X 3			8.7	91.7
12				
14			1.3	99.1
T.P.			-1.00	1199.42
	+10.97	1210.39		
15			3.2	07.2
T.P.			-0.09	1210.30
	+8.40	1218.70		
14				
13				

✓

33 — 3.3 - 6 — 10

-12.8 -12.7 -9.1 -0.1 0.0 -0.1 -6.9 -6.9

+2.0 +0.3 -1.5 -0.5 0.0 +0.1 -1.1 +2.5 +6.6

+3.0 +5.1 +4.6 -0.8 -0.1 0.0 +0.3 -0.8

-0.9 -0.3 0.0 -0.8 -1.6

-1.2 0.0 0.0 +0.1 -0.9

+0.7 +2.8 -0.5 00 0.0 0.0 -0.7 +3.4 +6.2

Sta.	B.S.	H.I.	F.S.	Elev.
	+12.06	1222.86		1210.30
16			6.7	15.7
			-0.66	1221.70
	+8.77	1230.47		
17			8.0	22.4
18			5.7	24.8
19			4.2	26.2
BM 3	+8.18	1230.73		1227.33
T.P.			-0.77	1229.66
20	+11.94	1241.60	11.2	30.4
21			6.6	35.0
22			4.0	37.6
T.P.			-2.19	1239.41
	+8.88	1248.29		
23			8.1	40.2

check on BM

✓

+3.0 +2.8 -0.2 +0.2 0.0 +0.2 -1.1 +1.7 +4.4
3.7 3.9 6.9 6.5 6.5 7.8 5.0 2.3
25. 9. 7. 6. 6.7 11. 13. 15. 25.

-1.1 +0.7 0.0 -0.8 -0.3 0.0 -0.2 -0.4 +1.5 +1.9
9.1 7.3 8.0 8.7 8.3 8.2 8.4 6.5 6.1
25. 12. 8. 9. 5. 8.0 10. 13. 18. 25.

+0.2 +0.3 -0.6 -0.2 0.0 -0.4 -1.0 +0.6 +0.8
5.4 5.3 6.2 5.8 6.0 6.6 5.0 4.8
25. 10. 6.4 8. 4. 5.6 9. 11.8 14. 16. 25.

+0.3 +1.1 00 0.0 -0.1 -0.5 +1.7 +2.1
3.9 3.1 4.2 4.3 4.7 2.5 2.1
25. 10. 9. 4.2 6. 5.4 10. 13. 25.

+0.2 +0.9 -0.4 -0.1 0.0 0.0 +1.8 +2.8
11.0 10.3 11.6 11.3 11.2 9.4 8.4
25. 12. 10. 6. 11.2 9. 12. 25.

-0.2 +0.4 -0.2 0.0 0.0 +0.2 +0.1 +1.9
6.8 6.2 6.3 6.6 6.4 6.8 4.7
25. 11 10 5. 6.6 8. 9. 25.

+0.8 +0.7 0.0 0.0 0.0 +2.0 +3.0
3.2 3.3 4.0 4.0 2.0 1.0
25. 9. 9. 10. 16. 25.

+1.1 +0.6 -0.3 0.0 0.0 0.0 -0.6 +1.9 +2.2
7.0 7.5 8.4 8.1 8.1 8.1 6.2 5.9
25. 15. 11. 12. 8 6. 9. 20. 25.

Sta.	B.S.	H.I.	F.S.	Elev.
		1248.31		
2+7			6.3	42.0
2.5			5.7	43.1
2.6			4.3	44.0
27			3.5	44.8
28			4.1	44.2
29			5.9	42.4
BM 4	+6.20	1248.31		1242.11
	+1.01	1243.12		
30	R.R. readings on bank of drive		2.9	40.7
	To Acreage Station			
31			4.9	38.2

✓

-0.4	-0.5	-1.4	-0.7	0.0	+0.1	-0.7	+0.2	+0.9	+1.0
6.7	6.8	7.7	7.0		6.2	7.0	6.1	5.4	5.3
25.	16.	14.	12.	6.3	9	10	12	13.	17. 25.
-0.6	-1.4	-1.3	-0.3	0.0	-0.4	-0.9	-0.0	+0.7	
5.8	6.6	6.5	5.5		5.6	6.1	5.2	4.5	
25 18.	15	12	10.	5.2	6.	9.	12	25.	
-0.4	-1.3	-0.2	+0.1	0.0	-0.3	-0.6	+0.8	+0.3	+0.8
4.7	5.6	4.5	4.2		4.6	4.9	3.5	4.0	3.5
25.8 17.	16.	11.	6.	4.3	4.	9.4	9.	11.	18. 25.
-0.7	-0.8	-1.6	-0.1	0.0	-0.5	-0.8	0.0	+0.5	
4.2	4.3	5.1	3.6		4.0	4.3	3.5	3.0	
25.	15	13.	6.	3.5	7	11.	12.	25.	
+0.3	+0.2	-1.5	-0.1	0.0	-0.1	-1.0	+0.9	+1.0	
3.8	3.9	5.6	4.2		4.2	5.1	3.2	3.1	
25.	14.	12	6.	4.1	4	9.	12.	25.	
-0.3	-0.1	-1.2	-0.1	0.0	-0.3	-1.1	+0.9	+1.4	
6.2	6.0	7.1	6.0		6.2	7.0	5.0	4.5	
25.	16.	13.	9.	5.9	4	9	12	25	
-0.6	-0.1	-1.2	-0.3	0.0	-0.8		+1.5	+2.0	
3.0	2.8	3.6	2.7		3.2	ditch	0.9	0.4	
25	15	12.	8.	2.4	10.		17.	25.	
-1.4	-1.0	-1.6	-0.4	+0.2	0.0	-0.2	-0.7	+0.1	+1.7
3	5.9	6.8	5.3	4.1		5.1	5.6	4.8	3.2
25.	17.	15.	11.	6.	4.9	3.	9.	11.	25.

Sta.	B.S.	H.I.	F.S.	Elev.
32		1243.12	8.7	34.4
33			12.8	30.3
T.P.			-11.89	1231.23
	+0.30	1231.53		
34			3.9	27.6
35.			5.9	25.6
36			7.4	24.1
37			9.1	22.4
38.			10.1	21.4
T.P. on E. Parapet			-8.94	1222.57
	+1.70	1224.29		
+49	Sec. Thru Culvert		3.4	20.9

+1.5 +1.6 -0.5 -0.1 +0.2 0.0 -0.3 -0.9 +2.8 +3.3
7.2/25. 7.1/16. 9.2/13. 8.8/10. 8.5/5. 8.7 9.0/5. 9.6/6&7 5.9/12. 5.4/25.

+3.2 +2.3 -0.4 -0.1 0.0 -0.2 -1.0 +2.1 +2.9
9.6/25. 10.5/17. 13.2/10. 12.9/7 12.8 13.0/5 13.8/7&9 10.7/12. 9.9/25.

+0.5 +0.1 -1.0 -0.3 0.0 -0.3 -0.8 +0.2 +0.3
3.4/22&25. 3.8/13. 4.9/10. 4.2/6. 3.9 4.2/6. 4.7/10&12. 3.7/14. 3.6/25.

-0.3 0.0 -0.8 -0.1 0.0 0.0 -0.7 -0.2 +1.3
6.2/23&25 5.9/11. 6.7/9. 6.0/6. 5.9 5.9/6. 6.6/9.7 10. 6.1/12. 4.6/25.

+0.1 +0.1 -0.6 -0.1 0.0 -0.1 -0.9 -0.2 +0.4
7.3/18&25 7.3/10. 8.0/7&9. 7.5/5. 7.4 7.5/6. 8.3/9&11. 7.6/13. 7.0/25.

-0.7 -0.2 -0.9 -0.1 0.0 -0.1 -0.7 -0.1 -0.8
9.8/20&25. 9.3/9. 10.0/7. 9.2/3. 9.1 9.2/7. 9.8/10. 9.2/14. 9.9/25.

+0.6 +0.4 -0.6 -0.3 0.0 -0.4 +1.0 +1.1
9.5 9.7/15. 10.7/8. 10.4/3 10.1 10.5/15. 9.1/21 9.0/25.

Stone Box Culvert 3½' x 4¼' x 18' Long (Good)
Condition good - [illegible]
×6.5 — × — 11.5 ×

-6.7 -5.1 +1.6 +0.2 0.0 +0.3 +1.7 -5.0 -4.1
10.1/28. 8.5/8. 1.8/7. 3.2/5. 3.4 3.1/10. 1.7/11. 8.4/12. 7.5/25.

7.5c

Sta.	B.S.	H.I.	F.S.	Elev.
		1224 29 (32) check on BM 5		
39			5.4	18.9
40			4.7	19.6
41			5.1	19.2
42			6.2	18.1
+13.7				
+13.7	xsec Through Sluice		6.6	17.7
+26	Approx. ℄ Road E. & W.		6.8	17.5
BM 5	+7.53	1224.32		1216.79
43			7.5	16.8
BM 5	+3.50	1220.59		
44			5.5	15.1

-2.9 -1.2 -0.6 -1.0 -0.3 0.0 0.0 -0.6 0.0 +1.2 +1.6

~~-2.6~~ ~~-0.9~~ ~~-0.3~~ ~~-0.7~~ ~~0.0~~ +0.3 ~~-0.3~~ ~~+0.3~~ ~~+1.5~~ ~~+1.9~~

8.3/26. 6.6/15. 6.0/10. 6.4/8. 5.7 5.4/10. 6.0/15. 5.4/16. 4.2/21. 3.8/25.
5.4

-0.3 +0.6 -0.5 -0.1 0.0 -0.1 -0.3 +0.9 +0.8 +1.6

5.0/25. 4.1/10. 5.2/6. 4.8/3. 4.7 4.8/8. 5.0/11. 3.8/14. 3.9/20. 3.1/25.

-0.6 +0.1 -0.4 0.0 0.0 -0.4 +0.8 +2.1

5.7/25. 5.0/6. 5.5/4. 5.1 5.1/10. 5.5/15. 4.3/15. 3.0/25.

+0.2 +0.4 0.0 -0.6 0.0 +0.4 +0.6 -0.2

6.0/25. 5.8/10. 6.2/5. 6.8/4. 6.2 5.8/9. 5.6/22. 6.4/23 & 25.

6.23" V.P. Sluice good condition Open

< 8.5' → 26.7 →

-2.6 -0.7 0.0 +1.2 -0.4

9.2/9. 7.3/6. 6.6 5.4/25. 2.0/27.

7.2 4.1 0.0 +2.0 +3.6

14.0/100. 10.9/50. 6.7 4.8/50. 3.2/100

-1.7 -1.2 -1.3 -0.2 +0.3 0.0 -0.6 +0.4 +0.5

9.2/25 8.7/20. 8.7/15. 7.7/10. 7.2/4. 7.5 8.1/34.7 7.1/9. 7.0/25.0

+0.2 -0.9 +0.1 0.0 -1.2 +0.9 +2.0

17.7 5.3/25. 6.4/16. 5.4/7. 5.5 6.7/5.47 4.6/9. 3.5/25.

Fuller
Grace
Thompson
Nov. 14th
1919

	1220.59	7.7	12.9
45		9.7	12.9
46		10.9	09.7
T.P.		−11.48	120.11
	+2.19	1211.28	
47		8.1	06.2
48		10.8	00.5
T.P.		−11.95	199.83
	+2.99	1202.32	
49		8.9	96.9
50		6.2	96.1
51		6.4	95.9
52		7.6	94.7

+0.9	−0.8	0.0	+0.1	0.0	−0.2	−1.7	+0.9	+2.4	
8.6	8.5	7.7	7.6	7.7	2.9	2.4	6.1	5.3	
25.	17.	10.	6	7.7	2.	5.	9.	25.	
	−0.9	−0.3	+0.2	0.0	−1.4	+1.7	+2.2	+3.3	
	11.5	11.2	10.7		12.3	9.2	8.7	2.6	
25.5	20.	16.	7.	10.9	4.	9.	20.	25.	
+0.3	+0.5	−0.6	+0.1	0.0	−0.7	+2.3	+3.4		
4.8	4.6	5.7	5.0	5.1	5.8	3.8	1.7		
25.	17.	12.	6.		5.	9.	25.		
+3.3	+3.0	−0.2	+0.1	0.0	−0.7	+3.7	+5.0		
7.5	7.8	11.0	10.7		11.5	2.1	5.8		
25.	17.	12.	6.	10.8	5.	12.	25.		
−1.6	−0.9	−0.4	0.0	0.0	+0.1	−0.4	−0.5	0.0	−0.5
7.0	6.3	5.8	5.4		5.3	5.8	5.9	5.7	5.9
25.	20.	9.	5.	5.9	8.	7.	12.	17.	25.
−2.3	−1.3	−0.3	0.0	−0.2	−1.0		+0.2	+0.6	
8.5	7.5	6.5		6.4	7.2		6.0	5.6	
25.	20.	6.0	6.2	6.	11.	12.	17.	25.	
−2.4	−0.5	−0.4	0.0	+0.1	+0.6	+1.6	+1.8		
8.8	6.9	6.8		6.3	5.5	4.8	4.6		
25.	11.	4	6.4	12.	12.	22.	25.		
	0.0	−0.4	0.0	0.0	+0.1	−0.3	+1.6	+1.8	+2.6
	7.6	8.0	7.6		7.8	7.9	6.0	5.8	5.0
18.8	26.	11.	6.	7.6	3.	7	12.	19.	25.

55		1202.32		12.2	90.1
	+0.87	1190 .95 97		-12.22	1190.10
54				7.0	84.0
+75 ✓				10.5	80.5
55	Bridge			11.1	79.9
+25 ✓				10.7	80.3
56				7.7	83.3 (1235.1)
B M #6	+5.83	1190.95			1185.12
BM	+6.71	1191.83			
+50 ✓				6.8	85.0
57				7.1	84.7

Check on B.M.

+1.9 +1.8 -0.4 0.0 -0.1 -0.7 +2.4 +3.9
25 10.3/23 10.4/14 12.6/11 12.2 12.3/7 12.9/7.0 9.8/12 8.3/25

+2.7 -0.9 0.0 0.0 -0.6 +3.8 +4.9
25 4.3/23 7.9/15 7.0/14 7.0 7.6/8 3.2/14 2.1/25

-2.1 -2.0 -0.4 0.0 -0.3 -2.0 -1.7 -2.6
12.6/25 12.5/17 10.9/12 10.5/7 10.8/8 12.5/13 12.2/20 13.1/25

Stone Box Culvert 2, 4' x 3' x 52 long. on top Stone

-14.8 -5.8 -3.6 -0.2 0.0 -0.1 -4.6 -12.6 -11.9
25.9/31 16.9/30 14.7/20 11.3/12 11.1 11.2/9 15.7/21 23.7/22 23.2/25
W. end on wall E. end on wall

W. end in bad shape E. end O.K.

-6.3 -2.8 -0.5 0.0 -0.1 -1.5 -2.4
17.0/26 13.5/17 11.2/12 10.7 10.8/9 12.2/17 13.1/25

+2.0 +1.9 -1.3 -0.3 0.0 -0.6 -1.4 +4.0
5.7/25 5.8/19 9.0/14 8.0/8 7.7 8.3/9 9.1/12 3.7/20 +25

+1.8 +2.0 -1.2 -0.5 -0.1 0.0 -0.5 -1.5 +2.2 +3.8
5.0/25 4.8/17 8.0/13 7.3/10 6.9/6 6.8 7.3/4 8.3/8 4.6/14 3.0/25

+2.5 +2.6 -1.1 -0.3 0.0 -0.2 +4.0 +4.8
4.6/27 4.5/17 8.2/12 7.4/10 7.1 7.3/5 3.1/16 2.3/25

58		1191.83	9.7	82.1
+050 ✓			11.2	80.6
TP	+3.75	1183.53	−12.05	1179.78
59			6.0	77.5
60			8.9	74.6
61			7.4	76.1
62	Sec. Taken at side of Drive on R42 for Coverage Sec.			79.3
+66 2/3				
63			4.1	79.4
64 0 0 2/3 ✓	Summit		3.0	80.5
64			6.3	77.2 ✓

+3.1 +3.4 −0.7 −0.1 0.0 −0.1 +3.8 +5.3

6.6 6.3 10.7 9.8 9.3 5.9 4.4
25. 16. 13 10. 9.7 5 12. 25

+2.3 +2.2 −1.3 −0.6 +0.2 0.0 −1.0 +2.5 +3.7

8.9 9.0 12.5 11.8 11.0 12.2 8.7 7.3
25. 21. 15. 12. 6. 11.2 7. 13. 25.

+2.9 +2.8 −1.4 −0.2 +0.3 0.0 0.0 −1.3 +2.8 +3.8

3.1 3.2 7.4 6.2 5.7 6.0 7.3 3.2 2.2
25. 22. 18.7 12 4 2. 7. 14. 25

Stone Box Culv. 3.8' × 5.6 × 28 Long

−16.1 −11.8 −1.8 −0.5 0.0 −0.3 −3.3 −7.6 −10.3

25.0 20.7 10.7 9.4 8.2 12.2 19.2
25. 14. 13. Top of wall 8. 8.9 10. 15. Top of wall 16.0

+0.7 +0.8 −0.8 −0.1 0.0 −0.4 −1.1 +1.4 +3.4

6.7 6.6 3.2 7.4 7.8 8.5 6.0 4.0 4.0
25 17. 14. 6. 7.4 9. 8. 11. 21. 25.

+0.4 +0.6 −0.8 0.0 0.0 −0.8 +1.4 +2.5

3.8 3.6 5.0 4.2 5.0 2.5 1.7
25 14. 13 7. 4.2 7. 14 25.

+0.6 +0.8 −1.1 0.0 0.0 −0.7 +1.7 +2.9

3.5 3.3 5.2 4.1 4.8 2.4 1.2
25. 14. 14. 11. 9.1 8. 15. 25.

0.0 +0.1 −1.2 0.0 0.0 −0.7 +1.1 +2.1

3.0 2.9 4.2 3.0 3.7 1.7 0.9
25. 15. 18. 5. 3.0 8 12. 23.

−1.1 −1.2 −1.7 −0.4 +0.2 0.0 −0.2 −0.4 +0.3 +1.1

7.4 4.5 5.0 6.7 6.1 6.3 6.5 6.7 6.0 5.2
25. 18 15 11. 6 5. 7. 11. 25.

65		1183	53	7.2	76.3
66				7.8	75.7
TP	+0.40	1177	66	-6.27	1177.26
67				2.9	75.0
68	12" tile in ditch line			3.6	74.1
+46					
+50					
69				6.4	71.3
+50 ✓				4.6	73.1
70				11.9	65.8
+25			68	-10.50	1169.16
	+5.52	1172	68		
71				10.0	62.7
+24					
+24				10.1	62.6 ✓

-0.3 -0.8 -1.8 -0.2 0.0 -0.4 -0.7 0.0 +1.4

7.5/25 8.0/18 9.0/17 7.4/9 9.2 7.6/4 7.9/7 7.2/8 5.8/25

-1.5 -1.5 -2.2 -1.1 -0.5 0.0 -0.5 +0.4 +0.8

9.3/25 9.3/18 10/17 8.9/13 8.3/10 7.5 8.3/7 7.4/14 7.0/25

-0.4 -1.0 -1.1 -1.8 -0.3 +0.1 0.0 -0.4 -0.9 +0.2 +1.1

3.1/25 3.7/21 3.8/18 4.5/17 3.0/10 2.6/5 2.7 3.1/6 3.6/9 2.5/14 1.6/25

+0.4 -0.2 -1.9 -0.8 -0.1 0.0 -0.2 -1.1 +0.8 +2.0

3.2/25 3.8/25, 21 3.5/18 4.4/15 3.7/11 3.6 3.8/4 4.7/6+8 2.8/14 1.6/25

6.7 12" tile ay.

+2.8 +2.5 -1.7 -0.1 0.0 (?) +1.7 +3.4 +4.6 +5.2

3.6/25 3.9/22 8.1/16 6.5/11 6.4 4.7/7 3.0/9 1.8/14 1.2/25

+1.3 -1.4 -0.6 +0.2 0.0 +0.9 +1.5 +2.1 +3.4

2.5 3.3/22 6.0/17 5.2/14 4.4/7 4.6 3.7/7 3.1/12 2.5/17 1.2/25

+1.7 +0.1 -1.5 -0.1 +0.2 0.0 -0.4 +4.8 +5.7 +5.8

10.2/24+25 11.8/20 13.4/18 11.8/16, 16 11.7/8 11.9 12.3/9 7.1/14 6.2/22 6.1/25

12" tile, 3' x, ends.

-4.9 -3.8 -1.1 -0.5 0.0 -0.5 -2.9 -2.1 -0.9

14.9/25 13.8/17 11.1/14 10.5/11 10.0 10.5/4 12.9/8 12.1/13 10.9/25

Stone Box Culvert 2 1/2' x 3' x 24' Long

-7.6 ← 16' → 0.0 -0.7 0.0 0.0 ← 8' → -0.5 +0.3 -7.9 -5.9

17.7/17 10.1/16 parallel 10.8/14 10.1/9 10.1 10.6/6 9.5/8.1 18/9 16.00/25

1178.9 | 19

72		1172	68	8.8	63.9
T. Rd s/t				-0.15	1172.53
					1172.53
+50	+10.99	1183.52		5.7	67.0
73				11.70	71.8
74				2.0	81.5
T.P.				-0.17	1183.35
	+3.32	1186.67	71=B.M.		
+60				2.8	83.9
B.M.#7	+8.00	x roads			1178.71
75				3.3	83.4
76				6.8	79.3
+32					
+32	→ use for veg. x sec. in Calculation			7.4	79.3

-1.4 -0.8 -2.0 -0.5 0.0 -0.2 -1.1 -2.1 -3.4

10.2/25 9.6/19 10.8/15+15 9.3/12 8.8 9.0/4 9.9/6 10.9/12 12.2/25

+4.0 +3.1 +0.3 -1.1 -0.3 0.0 -0.5 -1.7 0.0 +0.4 -1.6

1.7/25 2.6/21 5.4/15 6.8/13 6.0/10 5.7 6.2/6 7.4/9 5.7/11 5.3/15 7.3/25

+7.1 +6.5 -0.6 -0.3 0.0 -0.3 -1.5 +0.7 +1.4 +4.7

4.6/25 5.2/20 12.3/9 12.0/5 11.70 12.0/7 13.2/11 11./14 10.3/17 7.0/23+25

+4.0 -0.5 -0.3 0.0 -0.5 -1.1 +5.4

(H.I.+2.0 / 22+25) 2.5/12 2.3/7 2.0 2.5/7 3.1/10 H.I.+3.4/25

+4.1 +3.9 -0.7 -0.1 0.0 -1.0 +4.5 +4.6

H.I.+1.3/25 1.6/21 3.5/12 2.9/6 2.8 3.8/8 H.I.+1.7/21 H.I.+1.8/25

+3.3 +3.0 -1.3 -0.3 0.0 -0.5 -0.9 +2.0 +5.0

0.0/25 0.3/21 4.6/13 3.6/7 3.3 3.8/5 4.2/8 1.3/13 H.I.+1.7/25

-1.5 -1.2 -1.6 -0.3 0.0 -0.3 -0.8 +0.6 +2.4

8.3/25 8.0/14 8.4/13 7.1/5 6.8 7.1/5 7.6/11 6.2/17 4.4/25

12" V.P. Sluice fair cond.
9' x 12'

-1.6 -1.8 -2.2 -2.1 -0.8 0.0 +0.2 -1.8 +0.6

9.4/25 9.2/18 9.6/16 9.5/9 8.2/8 7.4 7.2/12 9.2/13 6.8/25

76		1156.91		
+60	x roads		7.7	79.0
+92				
+92			7.5	79.2
77			7.4	79.3
+8			5.4	81.3
79			2.3	84.4
T.P.			-1.79	1154.92
	+10.80	1195.72		
80			7.5	88.2
81			2.4	93.1
T.P.			-0.06	1195.66
	+11.75	1207.41		
82			10.40	97.0

✓

-2.6 -2.2 -1.6 0.0 +0.5 +1.7 +3.7

10.3 9.9 9.3 7.7 7.2 6.0 4.0
10.0 5.0 2.5 2.5 5.0 10.0

Stone Box Culvert. 3' wide & filled as stated

-4.3 -2.6 +0.2 +0.1 0.0 +0.2 +1.2 -3.2 -2.5

12.0 10.1 6.3 7.4 9.3 6.3 10.7 15.0
15.0 11. 10. 8. 7.5 11. 14 Parapet 15. 21

-2.7 -1.7 -0.9 -0.1 0.0 +0.1 -1.3 -1.7 -2.3

10.1 9.1 8.3 7.5 7.4 7.3 8.7 9.1 9.7
2.5 14. 12. 8 9. 14. 20. 2.5.

+1.3 +1.2 -0.4 -0.2 0.0 -0.1 -0.9 -1.1

4.1 4.2 5.8 5.6 5.4 5.5 6.3 6.5
2.5. 2.1. 14. 9. 6. 7. 2.5.

+0.9 +0.3 -0.7 -0.1 0.0 +0.1 -1.1 -0.2 +0.4

1.4 2.0 3.0 2.4 2.3 2.2 3.4 2.5 1.9
2.5. 15. 12. 10 9. 11. 15. 2.5.

+1.9 +1.8 -0.7 -0.2 0.0 -0.2 -1.3 +0.1 +0.5 +1.2

5.6 5.7 8.2 7.7 7.5 7.7 8.8 7.4 6.0 6.3
2.5. 18. 13. 10. 9. 11+12 14. 2.5 1.8

+1.1 +0.8 -0.4 -0.1 0.0 -0.3 -1.8 +0.1 +1.6

1.5 1.8 3.0 2.7 2.6 2.9 4.4 2.5 1.9
2.5. 16 11.0 6. 9 9+11. 14. 2.5.

+1.4 +0.4 -0.8 -0.4 0.0 -0.2 -1.6 +1.1 +1.5

9.0 10.2 11.2 10.7 10.4 10.6 12.0 9.3 8.9
2.5. 14. 10. 9. 7 8.7 12. 16. 2.5.

		1207.41		
83.			7.0	00.4
84			3.4	04.0
			-0.81	1206.90
	+10.26	1217.16		
86			10.7	06.8
87			7.6	09.6
88			6.9	10.5
89			5.2	12.0
90			3.8	13.4
			2.1	15.1
T.T.			-1.40	1215.76
	+11.36	1227.12		✓

+1.6 +0.6 -0.7 0.0 -0.2 -1.3 +1.4 +2.2

5.4/25. 6.4/13. 7.7/10. 2.0 2.2/7 8.3/10. 5.6/15. 4.8/25.

+0.7 +1.0 -0.4 0.0 -0.3 -1.1 +1.1 +1.8

2.7/25. 2.4/12. 3.8/9. 3.4 3.7/5. 4.3/6.7 2.3/14. 1.6/25.

+1.7 +2.4 -0.2 0.0 -0.1 -0.8 +1.0 +2.3

L. Bank (drive) 0.1–3.0

8.7/25. 8.0/18 10.6/10. 10.4 10.5/4 11.2/7. 9.4/11. 8.1/25.

+0.4 +0.3 -0.2 0.0 -0.2 -1.4 -0.4 +0.3

7.2/25. 7.3/13. 7.8/11. 7.6 7.8/8. 9.6/7.+9. 8.0/12. 2.3/25.

-1.0 -0.8 0.0 0.0 +0.1 -0.5 -0.6

7.7/25. 7.3/13. 6.7/9. 6.7 6.6/5. 7.2/7+9. 7.3/25.

-0.6 -0.8 +0.1 0.0 -0.1 -0.9 -0.4 +0.6

5.8/25. 6.0/13. 5.1/9. 5.2 5.3/7. 6.1/7. 5.6/9 4.6/25.

-0.5 -0.4 -0.8 -0.1 0.0 0.0 -0.6 -0.2 +0.1

4.3/23. 4.2/17. 1.6/15. 3.9/11. 3.8 3.8/31. 4.4/6.7 4.0/8. 3.7/25.

-0.5 -0.6 -0.9 -0.2 0.0 -0.1 -0.6 -0.3 -0.1

2.6/25. 2.7/18. 3.0/15. 2.3/9. 2.1 2.2/3. 2.7/6. 2.4/7. 2.2/25.

Fiedler
Grau
Thompson } Nov. 8th 1919

		1227.12		
91			10.0	17.1
92			7.8	19.3
93			5.0	22.1
94			1.7	25.4
TP	+3.97	1230.93 / 1230.91	−0.13	1226.94
95			2.5	28.4
BM # 8	+3.05	Sta. 96 (BM check)		1227.88
End of work Nov. 7 —				
96			6.3	24.6
	+0.16	1228.04		
97			6.5	21.5
98			9.0	19.0 ✓

76 + 12 + 24' L = BM   30 22

−0.3 −0.2 −0.6 0.0 0.0 −0.2 0.0
10.3/25 10.2/18 10.6/15 10.0/7 10.0 10.2/7 10.0/25

−0.1 −0.1 −0.8 −0.3 0.0 0.0 −0.3 +0.5 +1.4
7.9/25 7.9/16 8.6/14 8.1/13 7.8/7 7.8 8.1/4 + 6 7.3/9 6.4/25

−0.4 −1.0 −0.1 0.0 0.0 −0.3 +0.9 +1.8
25 5.4/16 6.0/15 5.1/13 5.0/10 5.0 5.3/5 4.1/8 3.2/25

+0.5 +0.2 −0.3 0.0 0.0 +0.6 +2.7
1.2/25 1.5/15 2.0/14 1.7/9 1.7 1.1/5 4.9/25 + 1.0

−0.7 −0.5 −0.1 0.0 +0.7 +1.3
3.2/25 3.0/12 2.6/7 2.5 1.8/15 1.2/25

+2.5 +1.2 +0.5 +0.3 0.0 0.0 −0.5 −0.1 +1.5 +2.8
3.8/25 5.1/12 5.8/10 6.0/6 6.3 6.3/0 6.8/8 6.4/10 4.8/18 3.5/25

−0.8 −0.6 −1.1 −0.2 0.0 0.0 −0.9 −0.1 +1.1
7.3/25 7.1/12 7.6/10 6.7/8 6.5 6.5/6 7.4/8 6.6/10 5.4/25

+0.2 +0.4 +0.2 −0.7 −0.3 0.0 −0.3 −0.5 +0.2 +1.6 +2.1
8.8/25 8.6/20 8.8/15 9.7/9 9.3/8 9.0 9.3/7 9.5/9 8.8/11 7.4/17 6.9/25

1228 04

99 — 11.6 — 16.4
T.P. — -11.90 — 1216.14

+1.05 — 12 17 19

100 — 5.9 — 11.3

101 — 10.5 — 06.4
T.P. — -12.28 — 1204.99

+0.11 — 12 05 10

102 — 6.0 — 99.1
(T.C. +51)

103 — 8.7 — 96.4

104 — 10.3 — 94.8
T.P. — -11.39 — 1193.71

+0.16 — 1193 87

105 — 2.3 — 91.6

106 — 7.5 — 84.4

✓

+0.5 +0.4 -0.6 0.0 -0.5 -1.7 +0.6 +1.5

11.2 / 2.5 — 11.2 / 11. — 12.2 / 9 — 11.6 — 12.1 / 9. — 13.0 / 9. — 11.9 / 14. — 10.1 / 25.

+2.4 +2.5 -1.8 -0.2 0.0 -0.6 -1.5 +2.4 +3.0

3.5 / 25. — 3.4 / 20. — 7.7 / 13. — 6.1 / 9. — 5 9 — 5.5 / 11. — 2.4 / 12. — 3.1 / 20 — 2.9 / 23

+1.4 +0.9 -0.2 0.0 -0.6 +0.6 +0.7

9.4 / 25. — 9.9 / 19. — 11.0 / 13. — 10 8 — 11.7 / 12. — 10.2 / 19 — 19.1 / 25

+1.6 +0.8 -0.2 0.0 0.0 +1.8 +1.5

4.4 / 25 — 5.2 / 12. — 6.7 / 8. — 6 0 — 6.0 / 11. — 5.2 / 16. — 4.3 / 25

-1.3 -0.6 -0.7 -0.2 0.0 +0.1 -0.6

10.0 / 25.0 — 9.3 / 11. — 9.4 / 9. — 8.9 / 8. — 8.7 — 8.6 / 12. — 9.3 / 25

-1.9 -1.4 -0.7 0.0 -0.1 -0.9 -0.2 -0.9

12.2 / 25 — 11.7 / 19. — 11.0 / 12. — 10 30 — 10.4 / 6. — 11.2 / 18. — 10.3 / 14. — 11.2 / 25

+2.8 +2.3 +1.5 -1.2 -0.5 0.0 -0.4 -1.7 -0.9 +0.9

H9+05 / 25. — 0.0 / 20 — 0.8 / 14 — 3.5 / 10 — 2.5 / 9. — 2.3 — 2.7 / 9 — 4.0 / 10. — 3.2 / 12. — 1.4 / 25

+4.5 +3.7 -0.1 0.0 -0.2 -1.2 +2.5 +2.1

3.0 / 25. — 5.8 / 14. — 2.6 / 9. — 9 5 — 9.7 / 16. — 10.7 / 7 — 7. / 12 — 7.4 / 25

		1193 87		
107	T.P.		-11.76	1182.11
		+0.78 1182.89		
107			7.6	75.3
		1110	-11.45	1171.44
		+0.92 1172.36		
108			6.4	66.0
		1110	-11.20	1161.16
		+0.07 1161.23		
109			4.0	57.2
110			9.4	51.8
+33 1/3	✓		10.2	51.0
110+10	N.W. Cor. W Parapet		-10.11	1151.12
T.P.			-7.10	1154.13
111	+6.90	1161.03	5.70	56.0
+33 1/3	✓		3.9	57.1
				✓

+7.4 +7.0

11.2/25. 11.6/18. 1187

-0.1	+0.3	0.0	-0.5	+1.6	+1.1	-0.2	
4.7/14.	2.3/8.	7.6	2.1/4.	6.0/10.	6.5/19.	25/25.	
+7.7	+5.7	-1.3	-0.6	0.0	-0.2	-1.2	+1.5	+0.4
43+1.3	0.7	7.7	7.0			6.6	7.6	4.8	6.0
25.	20.	18.	8.	6.4		7.	20.	14.	25
+5.0	+4.7	-1.5	-0.6	0.0	-0.4	-2.7	-3.5	
43+1.0	0.7	5.5	4.6		4.4	6.7	7.3	
25.	11	7	5.	4.0	5.	15.	25.	
-4.9	-4.2	-0.7	0.0	-0.4	-3.2	-3.6	
14.3/25.	13.6/15.	10.1/6.	9.4		9.8/7	12.6/15.	13.0/25.	
-3.6	-0.8	-1.5	-0.4	0.0	-0.8	+4.2	+4.8	
13.9	11.0/15.	11.9/12.	10.6/7.	10.2		11.0/11.	6.0/19.	5.4/25.	
+1.5	+2.0	-0.4	0.0	-0.7	+4.3	+5.0	
3.5/25.	3.0/12.	5.4/9.	5.0		5.7/7.	0.7/13.	0.0/25.	
+1.9	+2.2	-0.7	0.0	-0.8	+3.3	+4.7	
2.2/25.	1.7/12.	4.6/9.	3.9		4.9/9.	0.6/16.	43+0.8/25.	

112		1161.03	8.6	52.4
+5.0 ✓			14.4	46.6
T.P.			-12.06	1158.97
	+0.41	1159.38		
113			6.1	43.3
+0.5	N.W. Cor. W. Prop't Cor.		5.02	44.36
114			9.7	39.9
115			10.1	39.3
T.P.			-5.42	1173.96
	+10.86	1154.82		
116			10.3	44.5
+25 ✓			8.0	46.8
117			5.8	49.0
+33 1/3 ✓			6.5	48.3 ✓

+5.6 +5.7 -0.5 0.0 -0.2 -0.9 +5.7 +6.1

3.0 2.9 9.1 8.8 9.5 2.9 2.5
2.5 19. 9. 8.6 5. 10. 20. 25.

+7.4 -0.6 +0.1 0.0 0.0 -0.6 +0.7 0.0

7.0 15.0 14.3 14.4 15.0 13.7 14.4
25.0 14. 9. 14.4 8. 10. 16 25.

-2.0 -1.9 -0.5 0.0 -0.3 -0.4 +2.1

8.1 8.0 6.6 6.4 6.5 4.0
25. 23. 10. 6 8. 16 or 17 25

-4.1 -3.9 -0.2 0.0 +0.1 -1.2 +6.0

13.6 18.4 9.4 9.4 10.7 3.5
25. 12. 5. 9.5 8. 12. 25.

-2.9 -1.9 -1.2 0.0 -0.1 +1.6 +4.3

13 12.0 11.3 10.2 8.5 5.8
25. 18. 9. 10.1 18. 19. 25.

+1.3 +1.8 -0.6 0.0 -0.1 -1.2 +7.7

9.0 8.5 10.9 10.4 12.5 2.0
25. 17. 12. 10.3 4. 6. 2.

+0.2 -0.5 +1.4 -1.0 -0.5 0.0 -0.2 -1.8 +6.0 +6.6

7.5 7.5 6.6 4.0 8.5 8.2 9.5 2.0 1.4
25 18. 16. 11 9. 8.0 5. 5. 20. 26.

+0.7 +1.0 +1.7 -0.8 -0.2 0.0 +0.8 +5.3 +5.8

5.1 4.8 4.1 6.6 6.0 5.0 0.5 0 0
25. 18. 17. 12. 9. 5.8 9. 14 25.

+1.6 +2.5 -0.8 0.0 +0.4 +4.9 +6.1

4.9 4.0 2.3 6.5 6.1 1.6 0.4
25. 17. 14. 9. 14. 2 5.

117		1154 82		10.8	44.0
T.P.				-11.67	1143.15
	+0.09	1143 24			
+75	✓			6.3	36.9
119.				7.9	35.3
+50	✓			9.0	34.2
+50 N.W. Cor. W Parapet Culvert				9.44	33.80
120				8.5	34.7
121				3.1	46.1
T.P.				-0.83	1142.41
	+9.89	1152 38 check on BM			
BM #10	+6.80	1152.28			1145.13
122				5.2	47.1
+33 1/3	✓			3.3	49.0
T.P.				-4.67	1147.41 ✓

+3.0 +2.8 +3.4 -0.8 0.0 0.0 -1.5 +5.9 +7.0 +7.4
7.8/25 8.0/22 7.4/19 11.6/14 10.8 10.8/2 12.3/4 4.9/16 3.8/20 3.4/25

+1.9 +2.2 -1.2 -1.1 -0.1 0.0 -0.2 -1.7 +4.9
4.4/25 4.1/22 7.5/16 7.4/14 6.4/10 6.3 6.5/4 8.0/5 +11. 1.4/25

-5.4 -5.1 -0.3 0.0 -0.2 -1.7 -1.2
13.3/25 13.0/23 8.2/10 7.9 8.1/4 9.6/9 9.1/18 × 25

-9.4 -1.4 0.0 -1.4 -0.3
9.44/14 10.4/13 9.0 10.4/9 9.3/10

+1.7 +0.1 -1.2 -0.3 0.0 0.0 -0.3 -2.0 -0.1 -0.4 +4.1
6.8/25 8.4/20 9.7/13 8.8/10 8.5/6 8.5 8.8/4 10.5/7 8.6/11 8.9/16 4.4/25

+2.5 +2.2 +0.3 0.0 -0.1 -0.8 +3.1 +3.5
0.6/25 0.9/19 2.8/14 3.1 3.2/6 3.9/8 0.0/13 2.9+0.4/25

+0.4 +0.4 -0.7 -0.1 0.0 -0.4 -0.8 +1.0 +3.1 +3.6
4.8/25 4.8/18 5.9/15 5.3/6 5.2 5.6/4 6.0/6 4.2/9 2.1/17 1.6/25

+0.1 -0.1 -1.2 0.0 +0.1 0.0 -0.2 +2.2 +3.1
3.2/30 3.4/25 4.5/15 3.3/10 3.2/4 3.3 3.5/10 1.1/14 0.2/25

5-280 | 12233.3 | 2.3
10560
16733
15840
893

T.P.				1147.61
	+8.27	1155.88		
+78			7.0	48.9
℄ X Roads = +68.9			6.9	49.0
X rd + 50 N			6.0	49.9
X Rd + 100 N			6.5	49.4

✓

(−2.6 0.0 +1.0 +1.2) Not plotted
9.6/140 7.0 6.0/76 5.8/35

−4.6	−2.8	−1.9	0.0	+1.6	+3.0	+5.0
11.5/100	9.7/50	8.8/25	6.9	5.3/25	3.9/50	4.9/100

1924 Levels on
Chester Caves Hill

B.M.	0.27	1164	79		1164.52
T.P.	0.85	1154	04	11.60	1153.19
T.P.	1.76	1143	69	12.11	1141.93
5+27				11.43	32.26
6+00				9.9	33.8
7				5.8	37.9
T.P.	12.59	1155.	89	0.39	1143.30
8				8.8	47.1
T.P.	11.82	1167	01	0.70	1155.19
9				11.0	56.0
B.M. Ck.				2.49	1164.52
10				2.2	64.8
T.P.	12.32	1178	66	0.67	1166.34
11				4.0	74.7
T.P.	11.58	1190	08	0.16	1178.50
+50				11.5	78.6
12				T.P.	82.4
12+16				5.7	84.4

4-10-24 Fine
Hanna
Thompson
Douglass

Cucumber 9+88

Lt. ℄ Rt

H. rail C.&E.

-1.7 11.6/25 | -0.8 10.7/14 | -0.2 10.1/9 | 0.0 9.9 | -0.3 10.2/6 | -0.6 10.5/7-8 | -0.1 10.0/8 | +0.4 9.5/25

-3.4 9.2/25 | -2.5 8.3/22 | -1.1 6.9/14 | +0.6 5.2/9 | +0.4 5.4/8-6 | 0.0 5.8/3 | 0.0 5.8 | +0.6 5.2/8 | 0.0 5.8/16 | +0.2 5.6/25

-1.9 10.7/12 | -0.5 9.3/9 | -0.8 9.6/6 | 0.0 8.8/3 | 0.0 8.8 | -0.3 9.1/4.5 | +0.6 8.2/7.5 | -1.2 10.0/11

-1.6 12.6/12 | +0.1 10.9/9 | -0.4 11.4/4 | 0.0 11.0 | -0.2 11.2/4 | +0.8 10.2/8 | -1.0 12.0/12

-2.5 4.7/12 | +0.4 1.8/8 | -0.1 2.3/3 | 0.0 2.2 | +0.2 2.0/7 | +0.5 1.7/9.5 | -0.2 2.4/12

+0.6 3.4/14 | -1.0 5.0/9 | -0.2 4.2/7 | 0.0 4.0 | +0.3 3.7/7-9 | -0.7 4.7/11-12 | +2.7 1.3/15

Rock=11 | -0.5 12.0/11-8 | -0.1 11.6/7 | 0.0 11.5 | +0.2 11.3/7 | -1.4 12.9/9-10 | 10=Bank

bank | -0.5 8.2/10-9 | +0.3 7.4/7 | 0.0 7.7 | +0.3 7.4/7 | -1.0 8.7/8-9 | +0.3 7.4/10 | Bank

bank | -1.0 6.7/10-8 | -0.7 6.4/7 | -0.4 6.1/3 | 0.0 5.7 | -0.4 6.1/2 | -1.2 6.9/6 | -0.9 6.6/10 | bank

		1190 08		
T.P.	12.55	12 02 02	0.61	1189.47
13			10.9	91.1
14			3.3	98.7
T.P.	11.10	1212.73	0.39	1201.63
15			6.0	06.7
T.P	11.75	1224.44	0.04	1212.69
16			8.8	1.56
+75			2.9	21.5
17			2.2	22.2
T.P.	9.18	1231 11	2.51	1221.93
18			6.6	24.5
19			5.0	26.1
T.P.	10.38	1240 84	0.65	1230.16
20			10.2	30.6

✓

Rock / Bank

-0.4 0.0 0.0 -0.5 -0.2 -0.8

11.3 / 10-9 | 10.7 / 8 | 10.9 | 11.4 / 4 | 11.1 / 5-7 | 11.7 / 9-10 } bank

-0.6 -0.1 +0.1 -0.2 0.0 +0.2 -0.6

bank 3.9 / 11-10 | 3.4 / 9 | 3.2 / 6.5 | 3.5 / 5 | 3.3 | 3.1 / 8 | 3.9 / 9-10 bank

-0.1 +0.4 0.0 +0.2 +0.4 -0.4

bank 6.1 / 10-9 | 8- 5.6 / 3 | 6.0 | 5.0 / 2 | 5.6 / 8 | 6.4 / 10-11 bank

Sta. 15+35 Lt. ditch drains to Lt. (small ravine)

-0.5 -0.1 0.0 0.0 -1.2

bank 9.3 / 10-9 | 8.9 / 7 | 8.8 | 8.8 / 8 | 10.0 / 9-10 bank

-0.4 -0.2 +0.2 0.0 -0.1 -0.4 -0.1 -1.0

3.3 / 10-9 | 3.1 / 4 | 2.7 / 2 | 2.9 | 3.0 / 4 | 3.3 / 6 | 3.0 / 8 | 3.9 / 9-10 ✓

+0.1 +0.2 -0.1 -0.2 0.0 +0.1 0.0

2.1 / 11 | 2.0 / 8 | 2.3 / 7 | 2.4 / 2 | 2.2 | 2.1 / 6 | 2.2 / 9-11 ✓

+0.9 0.0 -0.6 +0.1 0.0 -0.1 -0.8 -0.6 +1.0

5.7 / 13.5 | 6.6 / 12-11 | 7.2 / 9-7 | 6.5 / 6 | 6.6 | 6.7 / 4 | 7.4 / 5.5 | 7.2 / 11 | 5.6 / 13

+1.3 +0.1 -0.3 0.0 -0.2 0.0 +1.9

3.7 / 13 | 4.9 / 11 | 5.3 / 4 | 5.0 | 5.2 / 6 | 4.0 / 7 | 3.1 / 10

+0.9 -0.6 -1.0 0.0 -0.1 +0.2 +1.9

9.3 / 12.5 | 10.8 / 10 | 11.2 / 5 | 10.2 | 10.3 / 5 | 10.0 / 8 | 8.3 / 11

4-10-'24 SLOPE STAKES (4 Snakes) 31

Sta	B.S.	H.I.	F.S.	Elev.
B.M. #1	3.59	1127 60		1124.01
1			Grd. 5.67	21.93
2			5.63	21.97
T.P.	9.58	1132 27	4.91	1122.69
3			5.66	22.61
4			5.31	26.96
5			0.35	31.92
T.P.	7.14	1139 40	0.01	1132.26
6			5.40	34.00
7			−0.60	1140.00
T.P.			6.01	1133.39

6-30-'24 Fair — Hanna Grau Sperry

S.P.	6.41	1139 80		1133.39
5+50			✓ 7.40	32.40
6			5.80	34.00

S.P.	7.92	1141 31		1133.39
5+50			✓ 8.91	32.40
6			✓ 7.09	34.22
+50			4.70	36.61
7			1.64	39.67

set → F1.2 / 13.0 — set → F0.4 / 14.5

5.67 / 5.67 / 1.2	F1.2 / 13.0	F1.8 / 12.0	F0.4 / 13.5	F0.4 / 14.5	3.67 / 3.67 / 0.4
5.63 / 5.63 / 0.90	F0.9 / 14.0	F0.7 / 13.0	F1.2 / 12.0	F1.0 / 13.0	5.63 / 5.63 / 1.0
9.66 / 1	C0.0 / 15.5	C0.5 / 14.5	C0.6 / 15.0	C0.8 / 16.0	9.66 / 9.66 / 0.8
5.31 / 5.31 / 1.2	F1.2 / 16.0	F0.9 / 13.0	C0.5 / 15.0	C0.6 / 16.0	5.31 / 5.31 / 0.6
0.35 / 2.99 / 2.64	F2.6 / 16.5	F2.2 / 11.5	F1.0 / 12.5	F0.5 / 13.5	0.35 / 0.85 / 0.5
5.40 / 5.40 / 1.0	F1.0 / 16.5	F1.0 / 14.5	0.0 / 16.0	0.0 / 17.0	5.40 / 5.40 / 1.0
−0.60 / 2.71 / 3.3	F3.3 / 15.5	F3.3 / 14.0	F1.8 / 12.0	F1.8 / 13.0	−0.60 / 1.12 / 1.8

Spike in N.W. post of milk stand.

1141.31

N.C.				✓ 7.14	34.17
+50				✓ 5.26	36.05
T.P.				✓ 2.27	39.04
T.P.	11.22	1151 83		0.70	1140.61
+50				✓ 8.53	43.30
8				✓ 4.03	47.80
T.P.	12.40	1163 62		0.61	1151.22
+50				✓ 11.32	52.30
9				✓ 6.82	56.80

100 N.C.

		1163 62			
9+50				↓ 2,32	61.30
T.P.1	10.42	1173	28	0.76	1162.86
10				↓ 7,48	65,80
+50				↓ 2,98	70,30
B.M.				↓ 8,77	1161.51
T.P.	11.56	1184	70	0.16	1173,12
11				↓ 10,00	74.70
+50				↓ 5.80	78.90
12				↓ 1.70	83.00
T.P.	12.91	1197	07	0.54	1184.16
+50				↓ 9.97	87.10
13				↓ 5,87	91,20
+50				↓ 1.77	95,30
T.P.	1155	1208	50	0.12	1196.95
14				↓ 9,10	99.48
+50				↓ 5.00	03.50
15				↓ 0.90	07.60
T.P.	12.58	1220	70	0.38	1208.12
+50				↓ 9,00	11,70
16			↓ set 5.00	4.90	1158.0
+50				0,94	1976
T.P.1	10,02	1229	78	0,94	1219.76
17			set 10 high	7,04	2274
+50				↓ 5.17	24.61
18				↓ 4.28	25,50
+50				↓ 3.34	26.44

		1229 78			
19				↓ 2,03	27.75
					27.33
B.M.1	2,51	1229	84	2,51	1227.27
+50				↓ 0,40	29.44
T.P.	6.85	1236	28	0.41	1229.43
20				↓ 4.78	31,50
+50				↓ 2,53	33,75

Slope Stakes

from page 29

1240 84

Sta				
21			5.61 ~~1235~~	1235.23
22			2.22	38.62
T.P.	8.37	1248 33	0.88	1239.96
23			6.93	41.40
24			5.33	43.00
25			4.33	44.00
26			3.43	44.90
T.P.	5.01	1249 11	4.23	1244.10
27			3.97	45.14
28			4.59	44.52
29			5.88	43.23
B.M.			6.93	1242.18 / 1242 11
S.P. (4-12-'24 Rain)	0.50	1242.61		1242.11
30			1.34	41.27
31			4.16	38.45

	stake set			stake set	
5.61 / 5.41 / 0.2	C 0.2 / 15.5	C 0.2 / 14.5	C 1.3 / 16.0	C 1.4 / 17.0	5.61 / 4.21 / 1.4
2.22 / 2.52 / 0.3	F 0.3 / 14.5	F 0.3 / 13.5	C 1.4 / 16.0	C 1.7 / 17.0	2.22 / 0.52 / 1.7
6.93 / 8.43 / 1.5	F 1.5 / 15.5	F 1.1 / 12.5	F 0.5 / 13.5	C 0.1 / 14.5	6.93 / 6.83 / 0.1
5.33 / 7.33 / 2.0	F 2.0 / 14.0	F 1.5 / 12.0	F 0.4 / 13.5	F 0.2 / 14.5	5.33 / 5.53 / 0.2
4.33 / 6.33 / 2.0	F 2.0 / 12.0	F 2.0 / 11	F 0.5 / 13.0	F 0.4 / 14	4.33 / 4.73 / 0.4
3.43 / 5.23 / 1.8	F 1.8 / 13.0	F 1.3 / 12	0.0 / 14	C 0.0 / 15.0	3.43 / 3.43 / 0.0
3.97 / 5.77 / 1.8	F 1.8 / 12.5	F 1.2 / 11.5	F 0.3 / 13.5	F 0.1 / 14.5	3.97 / 4.07 / 0.1
4.59 / 5.59 / 1.0	F 1.0 / 13.0	F 1.5 / 12.0	C 0.9 / 15.5	C 1.0 / 16.5	4.59 / 3.59 / 1
5.88 / 7.68 / 1.8	F 1.8 / 12.5	F 1.6 / 11.5	C 0.3 / 14.5	C 0.3 / 15.5	5.88 / 5.58 / 0.3
S.W. root 12" Maple					
1.34 / 3.04 / 1.7	F 1.7 / 13	F 1.5 / 12	F 0.4 / 13.5	F 0.2 / 14.5	1.34 / 1.54 / 0.2
~~4.16 / 3.26 / 0.9~~ 4.16 / 5.76 / 1.6	F 1.6 / 13.5	F 1.0 / 12.5	C 0.6 / 15	C 0.9 / 16.0	4.16 / 3.26 / 0.9

Hanna
Thompson
Doug 1963

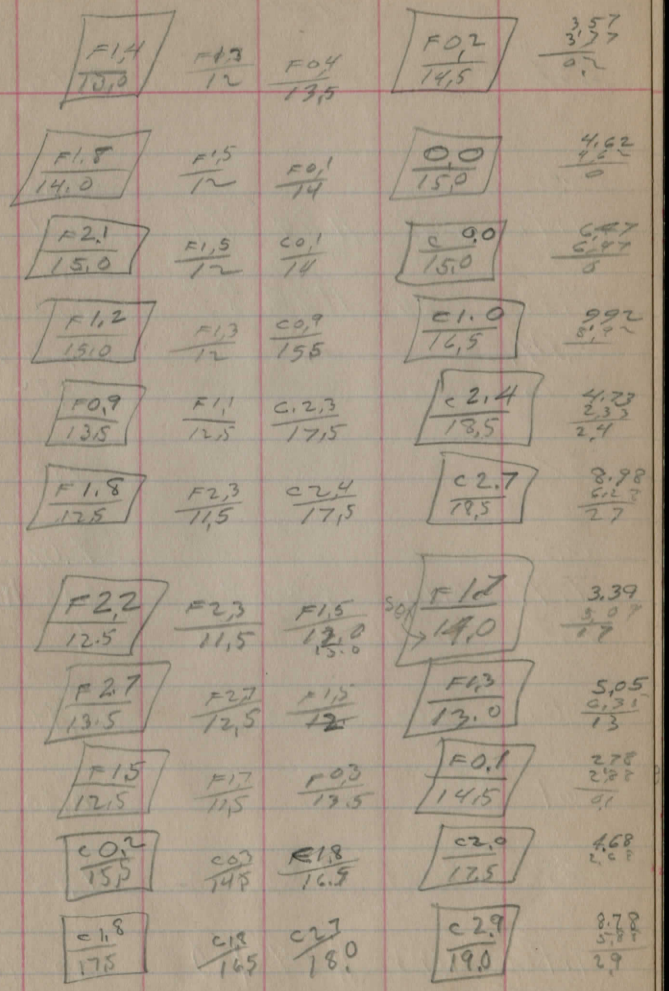
1242.61

32				7.65	34.96
33				10,98	31.63
T.P.	1.41	1231	19	12,83	1229,78
34				2.38	28.81
35				4.91	26.28
36				6.53	24.66
37				7.81	23.38
T.P.	0.55	1224	56	7.18	1224.01
38				2.22	22.34
39				3.27	21.29
40				4.31	20.25
41				5.36	19.20
42				6.41	18.15
T.P.	2.01	1220	67	5.90	1218.66
B.M.				3.90	1216.79
					1216.77

7.65 / 8.93 / 1.3	F1.3 / 13	F1.5 / 12	C2.7 / 18.0	C3.0 / 19.0	7.65 / 4.65 / 3.0
10.98 / 12.75 / 1.7	F1.4 / 12.5	F1.7 / 11.5	C0.9 / 15.5	C1.0 / 16.5	10.98 / 9.98 / 1
2.38 / 3.38 / 1	F1.0 / 13.5	F1.1 / 14.5	F1.0 / 12.5	F1.0 / 13.5	2.38 / 3.38 / 1
4.91 / 5.91 / 2.1	F0.3 / 14.0	F0.2 / 13	F0.8 / 13.0	F0.7 / 14.0	4.91 / 5.61 / 0.7
6.53 / 7.53 / 0.8	F0.8 / 13.5	F0.9 / 12.5	F0.7 / 13	F0.6 / 14.0	6.53 / 7.13 / 0.6
7.81 / 8.81 / 1	F1.0 / 13.5	F1.1 / 12.5	F1.5 / 12	F1.4 / 13.2	7.81 / 9.21 / 1.4
2.22 / 2.72 / 0.5	F0.5 / 14.0	F0.5 / 13	F1.4 / 12.1	F1.6 / 13.0	2.22 / 3.62 / 1.6
3.27 / 6.57 / 5.30	F3.3 / 14.6	F2.3 / 13.5	F2.5 / 12	F2.7 / 13.0	3.27 / 3.27 / 2.7
4.31 / 4.71 / 0.4	F0.4 / 14.0	F0.7 / 13	F0.6 / 13	C0.2 / 14.0	4.31 / 4.51 / 0.2
5.36 / 5.36	0.0 / 15.0	0.0 / 14	F0.2 / 14	C0.7 / 15.0	5.36 / 4.66 / 0.7
6.41 / 5.91 / 0.5	C0.5 / 15.5	C0.6 / 14.5		C0.2 / 20.5 set	6.41 / 5.81 / 0.6

1220 67

43			3,57	17.10	
44			4.62	16.05	
45			6,47	14.20	
46			9.92	10.75	
T.P.	1.66	1211	23	11.10	1209.57
47				4,73	00.50
48				8,98	02.25
T.P.	2.32	1202	25	1130	1199,73
49				3,39	98.86
50				5.05	97.20
T.P.	2.24	1199	18	5.31	1196.94
51				2,78	96.40
52				4.68	94.50
53				8,78	90.40
T.P.	2,32	1189	16	12,34	1186,84



		1189 16		
54			3.96	85.20
55			6.86	82.30
T.P.	5.22	1184 71	9.67	1179.49
55			2.41	82.30
T.P.	7.44	1189 82	2.33	1182.38
~~5.01~~			4.68	1185.14 / 1185.16
56			5.82	84.00
57			4.82	85.00
58			7.07	82.75
T.P.	0.10	1180 76	9.16	1180.66
59			1.76	79.00
60			4.99	75.77
61			3.60	77.16
62			1.44	79.32
T.P. / SP →	4.33	1184 10	0.99	1179.77

3.96 / 3.56 / 1.6	F1.6 / 13.0	F1.4 / 12	C3.3 / 19.0	C3.4 / 20.0	3.96 / 0.56 / 3.4
6.86 / 8.6 / 2.8	F2.8 / 14.0	F2.9 / 13		set at F6.9 / 18.5	~~4.86~~ 2.41 / 9.31 / 6.9
on Oak Lt.					
5.82 / 7.22 / 1.4	F1.4 / 12.5	F1.6 / 14.5	F1.7 / 11.6	F0.6 / 12.5	5.82 / 5.42 / 0.6
4.82 / 2.12 / 2.7	C2.7 / 19.0	C2.5 / 18.0	C4.3 / 20.5	C4.4 / 21.5	4.82 / 0.42 / 4.4
7.07 / 7.07	0.0 / 14.0	F0.7 / 13	C4.5 / 21	C4.7 / 22.0	7.07 / 2.37 / 4.7
1.76 / 3.96 / 2.2	F2.2 / 12.5	F1.7 / 11.5	F2.2 / 11.5	F2.0 / 12.5	1.76 / 3.76
4.99 / 7.69 / 2.7	F2.7 / 12.0	F2.5 / 11	set at →	F1.4 / 10.0	4.99 / 6.39 / 1.4
3.60 / 5.40 / 1.8	F1.8 / 12.0	F2.0 / 11	C1.1 / 15.5	C1.3 / 16.5	3.60 / 2.30 / 1.3
1.44 / 2.04 / 0.6	F0.6 / 13.5	F1.0 / 12.5	C0.1 / 14.5	C0.2 / 15.5	1.44 / 1.24 / 0.2

Blue on rock E. side of Rrive on Rt.

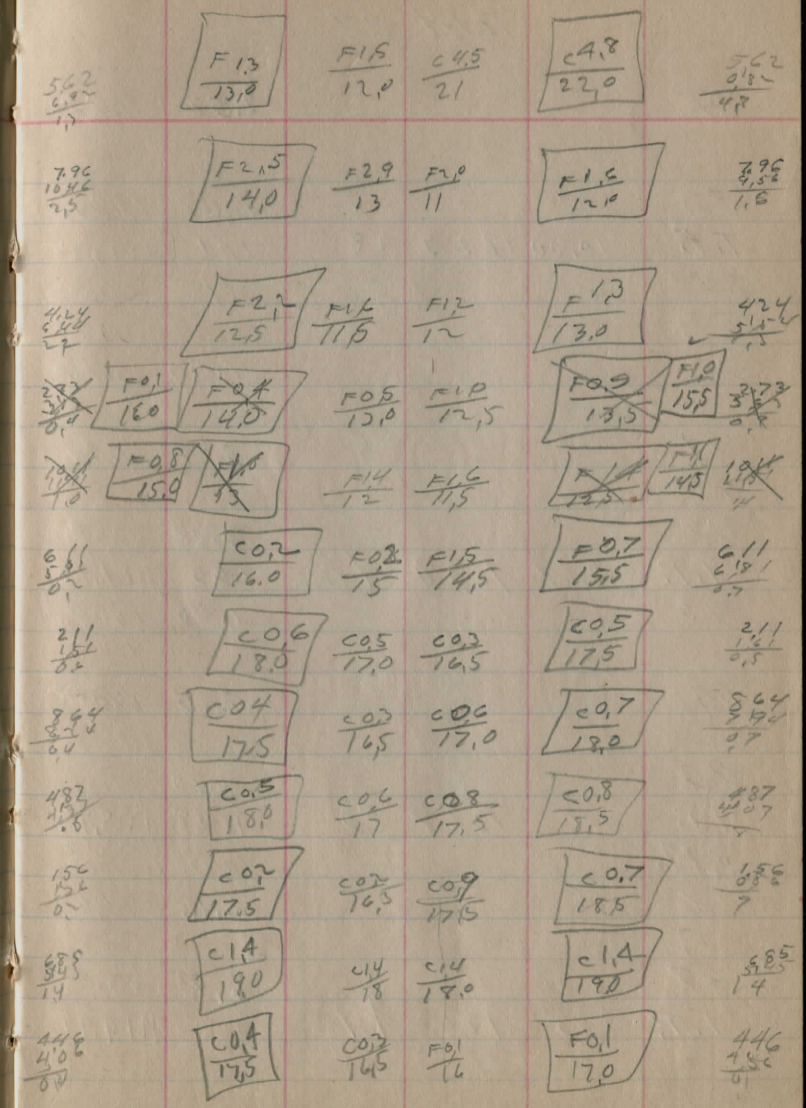
4-14-'24
Fair

		1184	10		
63				4.20	79.90
64				5.20	78.90
65				6.20	77.90
T.P.	1.59	1178	49	7.20	1176.90
66				1.59	76.90
67				2.59	75.90
68				3.84	74.65
69				6.73	71.76
T.P.	3.57	1171	91	10.15	1168.34
70				4.71	67.20
T.P.	6.15	1169	24	8.82	1163.09
71				5.33	63.91
72				3.40	65.84
T.P.	12.61	1181	28	0.57	1168.67
73				8.28	73.00
T.P.	9.15	1189	17	1.26	1180.02
74				8.25	80.92
~~T.P.~~ +60				5.95	83.22

Hanna
Thompson
Douglass

4.2 / 3.5 / 1.3	F1.3 / 13.0	F1.3 / 12.0	C1.6 / 16.5	C1.8 / 17.5	4.2 / 2.4 / 1.8
5.20 / 8.5 / 3.3	F3.3 / 15	F1.4 / 12	F1.0 / 12.5	F0.8 / 13.5	5.20 / 6.0 / 0.8
6.20 / 9.4 / 3.2	F / 13.5	F2.3 / 11.5	F1.1 / 12.5	F1.0 / 12.5	6.20 / 7.2 / 1
1.59 / 4.5 / 3	F3.0 / 16.0	F2.0 / 14.0	F0.3 / 13.5	F0.1 / 14.5	1.59 / 1.6 / 1
2.59 2.59 / 4.7 / 2.1	F2.2 / 17.0	F1.4 / 12	F0.7 / 13	F0.4 / 14.0	2.59 / 2.1 / 0.4
3.84 / 6.1 / 2.3	F2.3 / 16.5	F1.1 / 12.5	C0.3 / 14.5	C0.6 / 15.5	3.84 / 3.2 / 0.6
6.73 / 8.43 / 1.7	F1.7 / 15.5	F0.9 / 12.5	C4.1 / 17.0 1:1 slope	C4.3 / 18.0	6.73 / 2.43 / 4.3
4.71 / 7.5 / 2.8	F2.8 / 18.0	F0.7 / 12	C4.3 / 20.5	C4.3 / 21.5	4.71 / 0.4 / 4.3
5.33 / 8.33 / 3.0	F3.0 / 15.0	F1.5 / 12.0	F3.3 / 13.5	F3.4 / 14.6	5.33 / 8.73 / 3.4
3.40 / 5.9 / 2.5	F2.5 / 13.5	F2.1 / 11.5	F4.2 / 15.5	F4.2 / 16.5	3.40 / 7.6 / 4.2
8.28 / 2.58 / 5.7	C5.7 / 23.5	C5.6 / 22.5	F0.3 / 13.5	F0.1 / 14.5	8.28 / 8.37 / 0.1
8.25 / 3.45 / 4.8	C4.8 / 22.0	C4.8 / 21	C4.4 / 20.5	C4.9 / 21.5	8.25 / 3.35 / 4.9
5.95 / 1.75 / 4.2	C4.2 / 21.5	C4.5 / 20.5	C5.4 / 22.0	C5.3 / 23.0	5.95 / 0.65 / 5.3

		1189	17		
75				5.62	81.35
76				7.96	81.21
T.P.	5.76	1184	49	10.44	1178.77
3. M.	5.83	1184	54	5.83	1178.66
77				4.24	80.30
78				2.73	81.81
T.P.	12.58	1195	61	1.51	1183.03
79				10.11	85.50
80				6.11	89.50
81				2.11	93.50
T.P.	10.65	1206	14	0.12	1195.49
82				8.64	97.50
83				4.87	01.27
84				1.56	04.58
T.P.	9.83	1214	29	1.68	1204.46
85				6.85	07.42
86				4.46	09.83



		1214	29										
87				2,52	11.77	2.52 / 4.2 / 1.7	F1.8 / 12,5	F1.6 / 11,5	F1.6 / 11,5	F1.6 / 12,5	2.52 / 4.2 / 1.6		
88				1,07	13,25	10.4 / 3.0 / 2.0	F2.0 / 12,5	F1.8 / 11,5	F1.6 / 11,5	F1.4 / 12,5	10.4 / 2.40 / 1.4		
T.P.	10,00	1223	28	1,01	12 13,28								
89				8,78	14,50	8.78 / 10.78 / 2.0	F2.0 / 13,5	F1.2 / 12,5	F1.1 / 12,5	F1.0 / 13,5	8.78 / 1.70 / 1.0		
90				7.53	15,75	7.53 / 8.23 / 1.4	F1.4 / 13,5	F1.0 / 12,5	F0.9 / 12,5	F0.7 / 13,5	7.53 / 8.23 / 0.7		
91				5,84	17.44	5.84 / 6.84 / 1	F1.0 / 14,0	F0.8 / 13	F0.3 / 13,5	F0.2 / 14,5	5.84 / 6.04 / 0.2		
92				3,28	20.00	3.28 / 4.58 / 1.0	F4.3 / 13.5	F1.1 / 12.5	C0.3 / 14,5	C0.3 / 15.5	3.28 / 2.98 / 0.3		
T.P.	8.67	1230	40	1.55	1121,73								
93				7,46	23,00	7.40 / 8.90 / 1.5	F1.5 / 13,0	F1.4 / 12	C0.8 / 13,5	C0.8 / 14.5	7.40 / 5.5 / 1.5		
					?								
94				4.40	24,00	4.4 / 5.9 / 1.4	F0.9 / 13,5	F1,1 / 12,5	C1.3 / 16	C1.6 / 17,0	4.4 / 3.0 / 1.4		
95				2,90	27,50	2.9 / 2.5 / 0.4	C0.6 / 14,0	C0.5 / 15,0	C1.6 / 16.5	C 1.7 / 17,5	2.9 / 2.5 / 1.7		
T.P.	1.01	1229	93	1.48	1128,92 1227.90								
B.M.				2,03	1227.88								
96				3,93	26,00	3.93 / 4.43 / 2.05	C0.5 / 15,5	C0.3 / 14,5	F0.6 / 13	F0.4 / 14	3.93 / 4.13 / 0.4		
97				6,93	23.00	6.93 / 8.23 / 1.3	F1.7 / 13,0	F2.4 / 12	F1.4 / 12.	F1.3 / 13,0	6.93 / 8.23 / 1.3		
T.P.	2.23	1222	47	10.19	1219.74								

		1222 47										
98			2,47	20,00	2,47 / 3,23 / 0,76	F0,9 / 14,0	F0,5 / 13	C0,5 / 14,5	C0,6 / 15,5	2,47 / 1,87 / 0,6		
99			5,97	16,50	5,97 / 5,47 / 0,5	C0,5 / 17,5	C0,4 / 16,5	C0,9 / 17,5	C0,9 / 18,5	5,97 / 5,07 / 0,7		
100			10,47	12,00	10,47 / 12,35 / 1,9	F1,9 / 12,0	F2,0 / 11,0	F0,9 / 14,5	F0,7 / 15,5	10,47 / 11,17 / 0,7		
T.P.	2,10	1211 58	12,99	1209,98								
101			4,58	07,00	4,58 / 5,11 / 0,53	C0,1 / F0,1 / 16,5	F0,4 / 15,5	F1,2 / 14	F1,2 / 15	4,58 / 5,18 / 1,2	Blood Rock on Rt. 100+50	
102			9,58	02,00	9,58 / 11,41 / 1,9	F1,9 / 12,5	F2,2 / 11,5	F2,4 / 12,0	F2,0 / 13,0	9,58 / 11,58 / 2,00		
T.P.	0,79	1199 81	12,56	1199,02								
R.C.			-0,31	00,12	-0,31 / 2,89 / 2,60	F2,6 / 12,0	F2,6 / 11	F2,2 / 11,5	F1,9 / 12,5	-0,31 / 1,59 / 1,90		
103			2,37	97,44	2,37 / 5,17 / 2,8	F1,8 / 12,5	F1,8 / 11,5	F1,0 / 12,5	F1,0 / 13,5	2,37 / 5,37 / 1,0		
104			4,31	95,50	4,31 / 4,87 / 1,7	F1,7 / 12,5	F1,8 / 11,5	F1,7 / 12,0	F0,9 / 13,0	4,31 / 5,21 / 0,9		
T.P.	1,77	1194 53	7,05	1192,76								
105			2,38	92,15	2,38 / 4,16 / 1,7	C1,3 / 16,5	C0,9 / 15,5	F1,3 / 12	F0,8 / 13,0	2,38 / 3,18 / 0,8		
106			9,43	85,10	9,43 / 3,59 / 3,9	C3,9 / 20,5	C3,7 / 19,5	C1,9 / 17	C 2,0 / 18	9,43 / 7,43 / 2,0		
P.T.			13,22	81,31	13222 / 3,72 / 2,9	C6,0 / 24	C5,8 / 23	C3,4 / 19,0	C3,4 / 20,0	13,22 / 9,82 / 3,4		
T.P.	2,78	1184 26	13,05	1181,48								
107			8,06	76,20	806 / 6,4	C6,4 / 24,5	C6,3 / 23,5	F1,1 / 14,5	F1,1 / 13,5	8,06 / 9,16 / 1,1		
~~T.P.~~ T.P.	0,58	1172 00	12,82	1171,44							Spike in side of stump 107+75 Rt.	
~~0,58~~ SP.												
4												

		1172 00			
108				4.70	67.30
109				13.60	58.40
T.P.	1.24	1161 17		12.07	1159.93
109				2.77	58.40
B.M.	7.67	1161 25		7.67	1153.50 53.58
110				8.68 ~~8.60~~	52.57
T.P.	7.28	1161 43		7.10	1154.15
111				4.43	57.00
+50				4.63	56.80
112				8.79	52.64
T.P.	1.96	1150 36		13.03	1148.40
P.C.				4.29	46.07
113				6.87	44.49
T.P.	1.73	1143.79		8.00	1142.06
114				3.62	40.17
115				2.62	41.17
T.P.	10.79	1152 72		1.86	1141.93
116				6.72	46.00
T.P.	8.22	1157 45		3.49	1149.23
117				8.00	49.45

4.70 / 4.1 / .6	F 1.4 / 13.0	F 2.4 / 12	C 0.2 / 14.5	C 0.2 / 15.5	4.70 / 4.50 / .2
13.60 / 10.60 / 3.0	C 3.0 / 14.5	C 3.0 / 18.5	c		
			F 3.2 / 13.5	F 3.4 / 14.5	2.77 / 6.17 / 3.4
8.68 / 12.78 / 4.1	F 4.1 set at 13		F 3.2 / 13.5	F 3.7 / 14.5	8.68 / 12.13 / 3.7
4.43 / 3.43 / 1.0	C 1.0 / 16.5	C 0.9 / 15.5	C 3.8 / 20	C 4.0 / 21.0	4.43 / 0.43 / 4
4.63 / 2.63 / 2.0	C 2.0 / 18.0	C 2.0 / 17	C 3.8 / 20	C 4.0 / 21.0	4.63 / 0.63 / 4
8.79 / 3.29 / 5.5	C 5.5 / 23.0	C 5.5 / 22	C 5.6 / 22.5	C 5.7 / 23.5	8.79 / 3.09 / 5.7
~~4.29~~ / 6.79 / 2.5	F 2.5 / 12.5	F 2.6 / 11.5	F 2.0 / 11	F 1.9 / 12.0	4.29 / 6.19 / 1.9
~~11.87~~ / 1					~~11.87~~ / 1

Blue on side of headwalls.

3.62 / 7.8 / 4.2	F 4.2 / 13.0	F 4.4 / 14	F 0.4 / 13.5	C 0.6 / 14.5	3.62 / 3.02 / 0.6
2.62 / 5.82 / 3.2	F 3.2 / 14.0	F 2.9 / 13	F 1.0 / 14.5	F 0.6 / 13.5	2.62 / 3.2 / 0.6
6.72 / 7.42 / 0.7	F 0.7 / 13.0	F 1.2 / 12	C 2.3 / 17.5	C 2.5 / 18.5	6.72 / 4.2 / 2.5
8.00 / 8.6	F 0.6 / 13.0	F 1.3 / 12	C 6.0 / 23	C 6. / 24.0	8.00 / 2.00 / 6.0

		1157	45		
118				13.6.5	43.80
T.P.	6.10	1151	98	11.57	1145.88
118				8.118	43.80
T.P.	1.90	1141	46	12.42	1139.56
119				4.59	36.87
120				5.31	36.15
T.P.	1.81	1151	24	1.03	1140.43
121				9.61	41.63
122				3.86	47.38
B.M.				5.68	1145.56 1145.43

~~13.65~~			set at 255 / C7,6 stake		13,65 / 6,05 / 7,6
8.18 / 8.98 / 0,8	F0,8 / 13,5	F1,0 / 12,5			
	F2,5 / 12,5	F2,2 / 11,5	F2,8 / 12,5	F2,9 / 13,5	
4.59 / 7.09 / 2.5					4.59 / 7.49 / 2,9
5.31 / 7.31 / 2,0	F2,0 / 12,0	F2,0 / 11	F1,6 / 11,5	F1,9 / 12,5	5.31 / 7.2 / 1,9
	F2,1 / 12,5	F1,8 / 11,5	C1,6 / 16,5	C,1,7 / 17,5	
9.61 / 11.71 / 2,1					9.61 / 7.91 / 1,7
3.86 / 5.16 / 1,3	F1,3 / 14,5	F1,0 / 12,5	C3,8 / 18,5	C3,1 / 19,5	3.86 / 0.66 / 3,2

4-15-24
cold

Grades on Hill for concrete section

S.P.	9.29	1142 68			1133.39	Spike in N.W. post. milk stand
5+50			Marked 2.0↓	10.28	32.40	Berm stake 10' from ℄ Rt.
6			Grd.	8.51	34.17	" " " " " "
7			Grd.	3.64	39.04	" " " "
T.P.	12.36	1153 63		1.41	1141.27	
8			Grd.	5.83	47.80	" " "
T.P.	12.44	1165 77		0.30	1153.33	" " "
9			Grd.	8.97	56.80	
B.M.	11.08	1175 60		1.21	1164.56 1164.52	"
10			Grd	9.80	65.80	" " " " "
~~T.P.~~						
11			Grd.	1.00	74.60	" " " " "
T.P.	12.55	1187 91		0.24	1175.36	
12			Grd	4.91	83.00	" iron stake " "
T.P.	12.47	1199 19		1.19	1186.72	
13			Grd.	7.99	91.20	Iron " " " "
T.P.	12.39	1210 63		0.95	1198.24	
14			Grd	11.23	99.40	Iron 10 55' Rt
15			Grd.	3.03	07.60	Iron 11 2 Rt.
T.P.	12.29	1221 76		1.66	1208.97	
16			Grd.	5.96	15.80	Iron 10 6 Rt.
T.P.	7.32	1228 40		0.68	1221.08	

16+75		1228	40	7.01	21.39
				5.66	74
17				6.08	22.32
18				2.90	25.50
T.P.	7.22	1234	55	1.01	1227.39
					27.83
19				6.80	27.75
20				3.05	31.50
	9.42	1236	75		1227.33
20+50				3.00	33.75
21					36.00
T.P.	3.54	1212	53		1208.97
Culvert					
15+27					1209.81
					07.51

Grd. 5.02 (0.02 / 5.0)

Stake on RH = FL. → 5.0

Stake on LH. = FL. → 5.82 / 5.82 / 5.0

06.71

5.66 / 5.02 / 5.1	C 0.7 / 17.5	C 0.5 / 16.5	C 1.5 / 18	C 1.6 / 1.9	5.66 / 5.0 / 1.6
2.90 / 2.80 / 0.1	F 0.1 / 17.0	0.0 / 16.0	0.0 / 16.0	C 0.1 / 17.0	2.90 / 2.80 / 0.1
B. M. L.H. 6.80 / 6.3 / 0.5	F 0.4 / 16.5	F 0.4 / 15.5	C 0.4 / 16.5	C 0.5 / 17.5	6.80 / 6.3 / 0.5
3.05 / 3.0 / 0.1	F 0.1 / 17.0	F 0.2 / 16	C 2.0 / Tap	C 2.1 / 20	3.05 / 3.0 / 0.1
3.00 / 2.50 / 0.5	C 0.5 / 17.5	C 0.5 / 16.5	C 1.3 / 18	C 1.5 / 19	3.00 / 1.5 / 1.5

℄ Grd.

E. FL.

Elev.

Elev.

N. E. L.

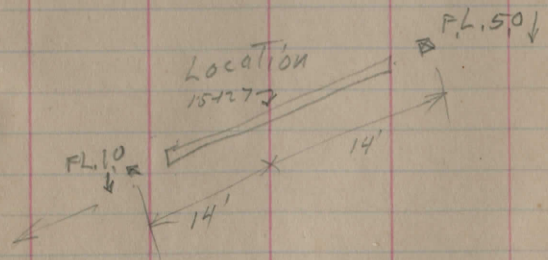


TABLE OF INCHES REDUCED TO DECIMALS OF A FOOT.

Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.	Ins.	Dec.
		1 5/16	.1094	2 9/16	.2135	3 13/16	.3177	5 1/16	.4219	6 5/16	.5260	7 9/16	.6302	8 13/16	.7344	10 1/16	.8385	11 5/16	.9427
		1/8	.1146	5/8	.2188	7/8	.3229	1/8	.4271	3/8	.5313	5/8	.6354	7/8	.7396	1/8	.8438	3/8	.9479
		1 1/16	.1198	11/16	.2240	15/16	.3281	3/16	.4323	7/16	.5365	11/16	.6406	15/16	.7448	3/16	.8490	7/16	.9531
		1/4	.1250	3/4	.2292	4—	.3333	1/4	.4375	1/2	.5417	3/4	.6458	9—	.7500	1/4	.8542	1/2	.9583
		5/16	.1302	13/16	.2344	1/16	.3385	5/16	.4427	9/16	.5469	13/16	.6510	1/16	.7552	5/16	.8594	9/16	.9635
		3/8	.1354	7/8	.2396	1/8	.3438	3/8	.4479	5/8	.5521	7/8	.6563	1/8	.7604	3/8	.8646	5/8	.9688
		7/16	.1406	15/16	.2448	3/16	.3490	7/16	.4531	11/16	.5573	15/16	.6615	3/16	.7656	7/16	.8698	11/16	.9740
		1/2	.1458	3—	.2500	1/4	.3542	1/2	.4583	3/4	.5625	8—	.6667	1/4	.7708	1/2	.8750	3/4	.9792
		9/16	.1510	1/16	.2552	5/16	.3594	9/16	.4635	13/16	.5677	1/16	.6719	5/16	.7760	9/16	.8802	13/16	9844
		5/8	.1563	1/8	.2604	3/8	.3646	5/8	.4688	7/8	.5729	1/8	.6771	3/8	.7813	5/8	.8854	7/8	.9896
		11/16	.1615	3/16	.2656	7/16	.3698	11/16	.4740	15/16	.5781	3/16	.6823	7/16	.7865	11/16	.8906	15/16	.9948
		3/4	.1667	1/4	.2708	1/2	.3750	3/4	.4792	7—	.5833	1/4	.6875	1/2	.7917	3/4	.8958		
		13/16	.1719	5/16	.2760	9/16	.3803	13/16	.4844	1/16	.5885	5/16	.6927	9/16	.7969	13/16	.9010		
		7/8	.1771	3/8	.2813	5/8	.3854	7/8	.4896	1/8	.5938	3/8	.6979	5/8	.8021	7/8	.9063		
		15/16	.1823	7/16	.2865	11/16	.3906	15/16	4948	3/16	.5990	7/16	.7031	11/16	.8073	15/16	.9115		
		1/4	.1875	1/2	.2917	3/4	.3958	6—	.5000	1/4	.6042	1/2	.7083	3/4	.8125	11—	.9167		
		5/16	.1927	9/16	.2969	13/16	.4010	1/16	.5052	5/16	.6094	9/16	.7135	13/16	.8177	1/16	.9219		
		3/8	.1979	5/8	.3021	7/8	.4063	1/8	.5104	3/8	.6146	5/8	.7188	7/8	.8229	1/8	.9271		
		7/16	.2031	11/16	.3073	15/16	.4115	3/16	.5156	7/16	.6198	11/16	.7240	15/16	.8281	3/16	.9323		
		1/2	.2083	3/4	.3125	5—	.4167	1/4	.5208	1/2	.6250	3/4	.7292	10—	.8333	1/4	.9375		

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
DRAWING MATERIALS AND SURVEYING INSTRUMENTS